

# Producing Zirconium Diboride Components with Complex, Near-Net Shape Geometries by Aqueous Room- Temperature Injection Molding

Valerie Wiesner

Profs. Jeffrey Youngblood and Rodney Trice

*Purdue University  
School of Materials Engineering*



NSF Materials and Surface Engineering Grant CMMI-0726304  
*NASA Pathways Program*, NASA Glenn Research Center  
U.S. Dept. of Education GAANN Grant P200A10036



# Advancing Ceramic Processing for Hypersonics

- Need for manufacturing complex-shaped ceramic components in aerospace
- Hypersonic flight speeds > Mach 5
  - Temperatures > 1900°C (3500°F)



NASA's X-43A hypersonic vehicle.

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Material	Melting Temperature (°C)	Density (g/cm³)	Flexural Strength (MPa)	Elastic Modulus (GPa)
ZrB <sub>2</sub>	3245	6.08	275-490	489-493
SiC	Dissociates 2245	3.21	480-580	410-444
Al <sub>2</sub> O <sub>3</sub>	2072	3.9	200-700	393
Stainless Steel AISI316L	1400	8	515-620	193
Aluminum 7075	900	2.8	228-572	71

Opeka, M.M., et al., *Journal of the European Ceramic Society*, 1999. 19(13-14): p. 2405-2414.

Fahrenholz, W.G., et al., *Journal of the American Ceramic Society*, 2007. 90(5): p. 1347-1364.

Callister Jr., W. D., *Materials Science and Engineering An Introduction*. John Wiley & Sons, Inc.: 2007; Vol. 7<sup>th</sup>.

# Advancing Ceramic Processing

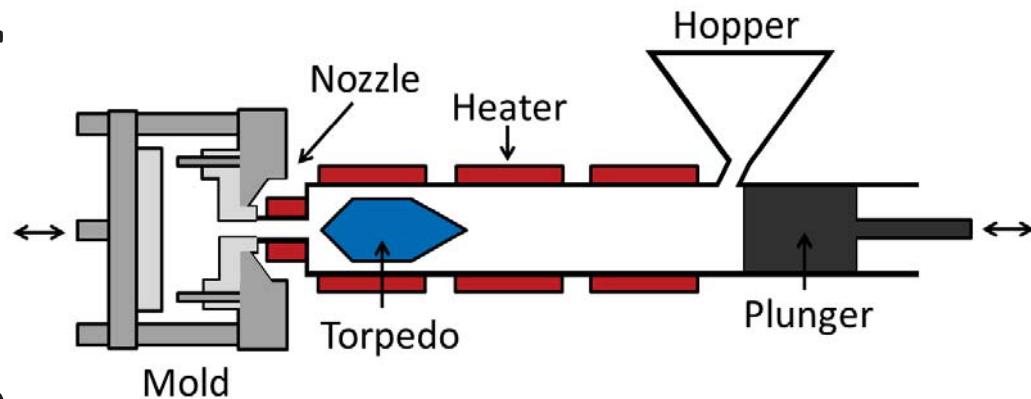
- Ceramic injection molding
  - Net-shape production of parts possible
  - High-volume production
  - Pressureless sintering



Parts fabricated by injection molding powders.

# Previous Work on Ceramic Injection Molding

- **Ceramic injection molding**
  - Net-shape production of parts possible
  - High-volume production
  - Pressureless sintering
- **Polymer-based binder system in feedstock**
  - Thermoplastic polymer
  - Wax (carnauba, paraffin)
  - Plasticizer or dispersant



Schematic of conventional plunger-type injection molding apparatus.

# Previous Work on Ceramic Injection Molding

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  - Thermoplastic polymer
  - Wax (carnauba, paraffin)
  - Stearic acid

→ Energy-intensive heating and cooling of feedstock

→ Non-aqueous, multi-component binders

# Ceramic Suspension Gel (CeraSGel)

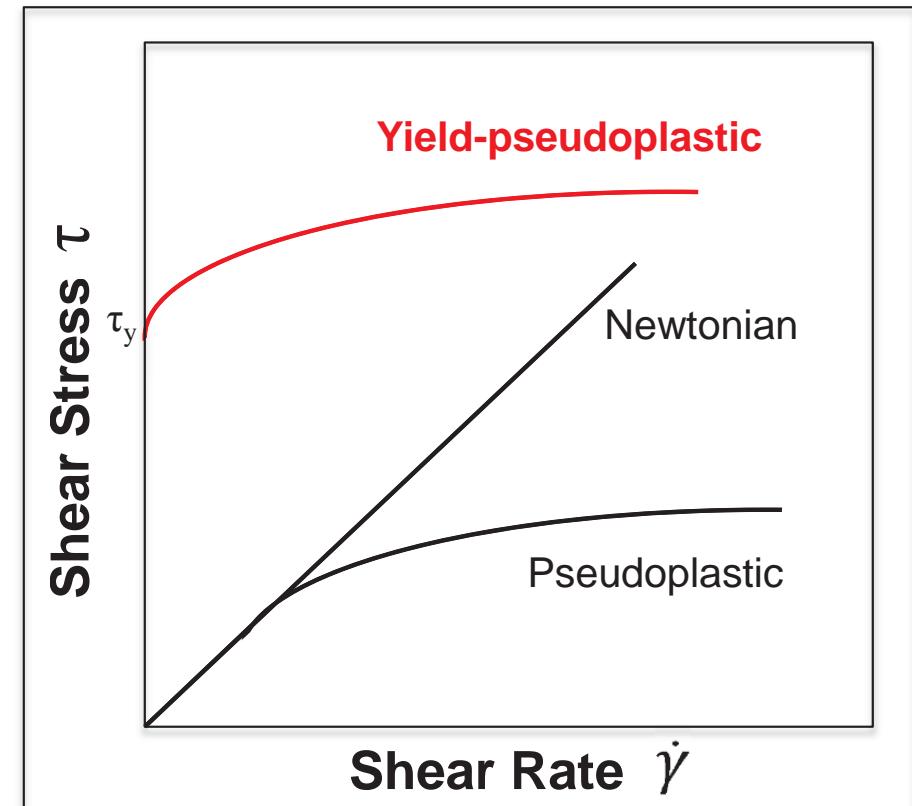
- Suspension of ceramic powders in polymer gel
  - High ceramic content (~50 vol.%)
  - Minimal addition of water-soluble polymer (<5 vol.%)

## Advantages

- Flowable at room temperature
- Yield-pseudoplastic
  - High yield point
  - Shear thinning

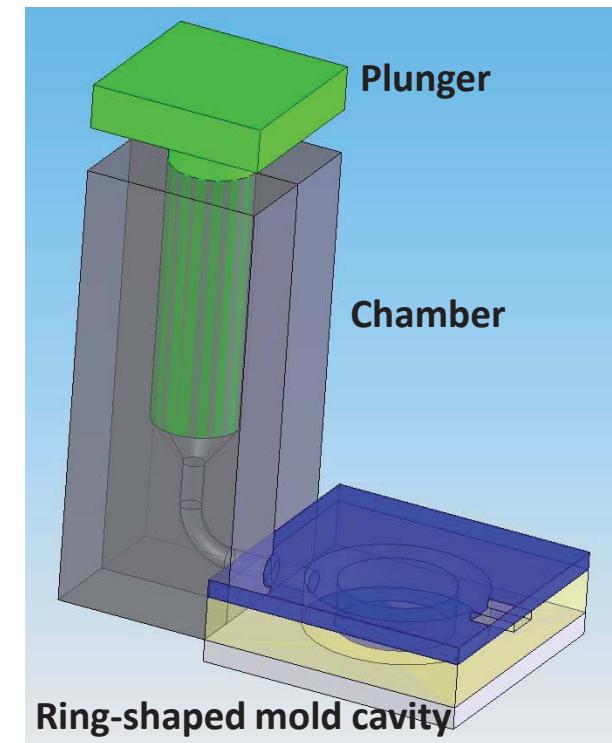
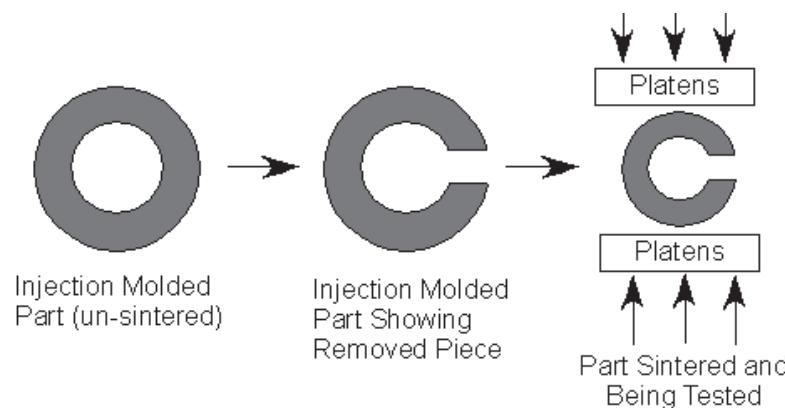


Sintered  $\text{ZrB}_2$  specimen (right) formed by casting CeraSGels.



# Injection Mold Design and Setup

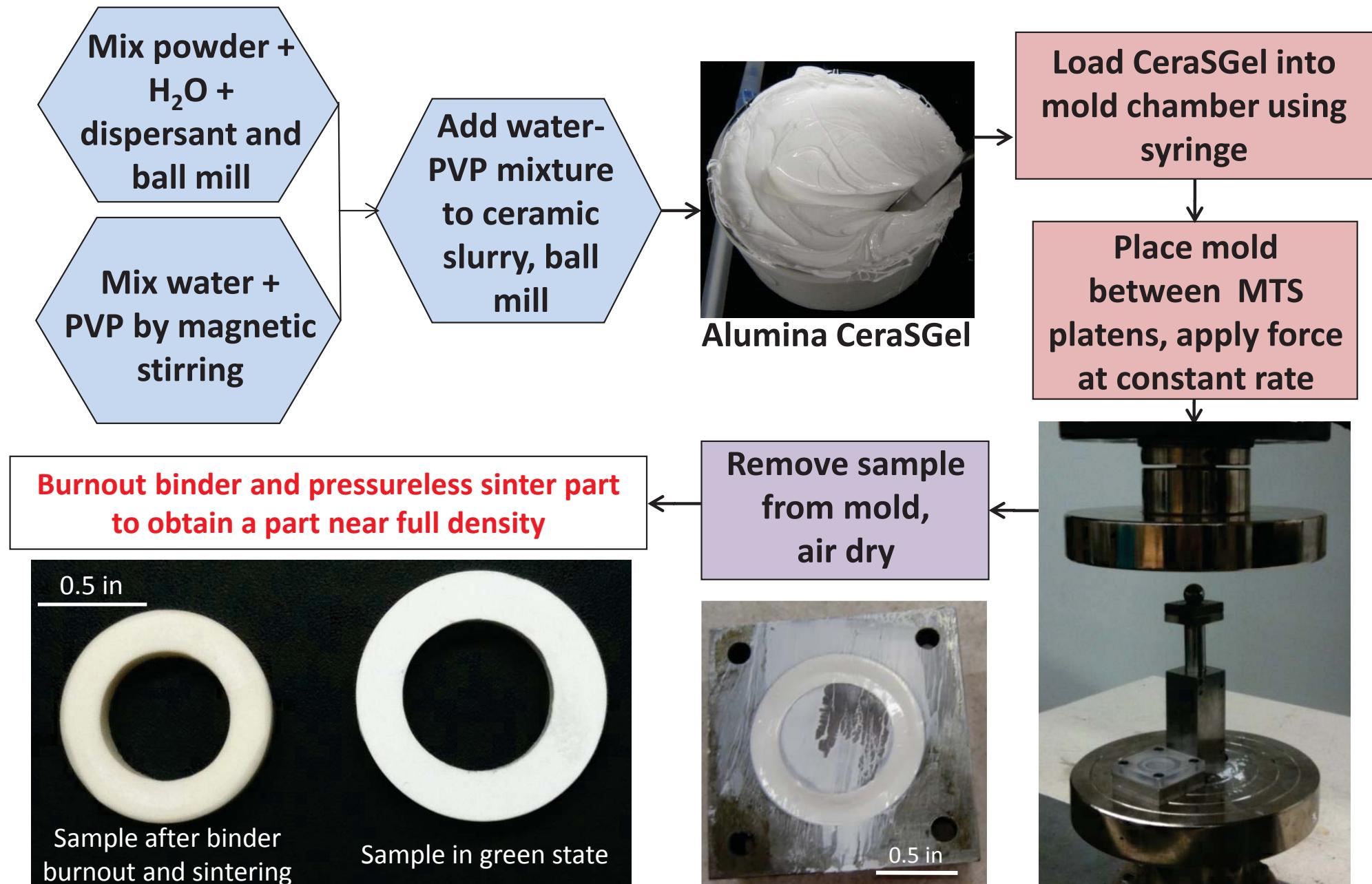
- Force at constant rate exerted onto plunger to force CeraSGel out of chamber into mold
  - MTS setup
- Mold design
  - Mechanical characterization using ASTM C1323-10



Schematic of injection mold device.

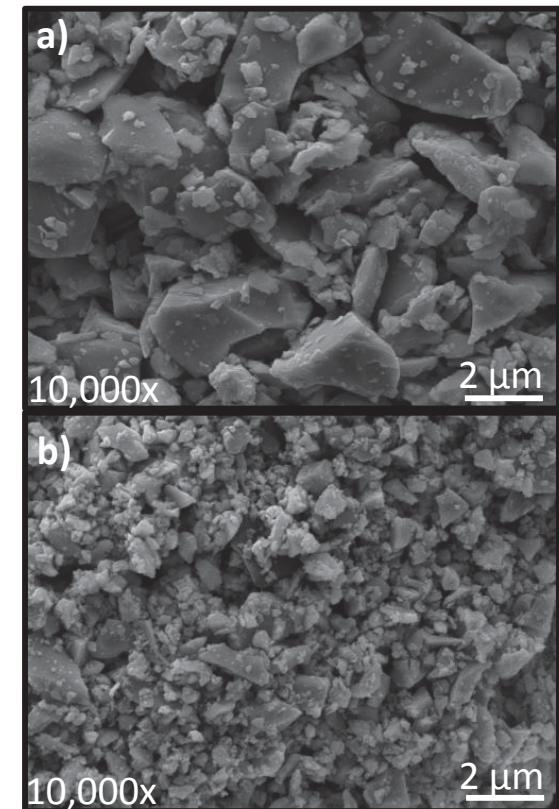
- Machine C-shape from ring

# CeraSGel Injection Molding Process



# ZrB<sub>2</sub> CeraSGel Material Selection

- *Pressureless sintering* of ZrB<sub>2</sub> typically >2000°C
  - ZrB<sub>2</sub> sensitive to oxygen impurities
  - B<sub>4</sub>C sintering aid
  - Attrition mill using WC media
- Dispersant to maximize ZrB<sub>2</sub> powder loading
- PVP as binder to tailor flow properties



SEM images of a) as-received ZrB<sub>2</sub> powders (H.C. Starck Grade B); b) ZrB<sub>2</sub>+B<sub>4</sub>C powders after attrition milling with WC media resulting in d<sub>50</sub>~0.5 μm.

# Characterizing CeraSGel Formulations

Evaluate effect of PVP content in CeraSGels containing 48.6 vol.%  $\text{ZrB}_2+\text{B}_4\text{C}+\text{WC}$

- 1 vol.% PVP
- 2 vol.% PVP
- 3 vol.% PVP

- Rheological behavior of CeraSGels
- Machinability in green state
- Density and composition after binder removal and pressureless sintering
- Mechanical strength of sintered samples

# Rheological Dependence on Polymer Content

## Vary PVP amount in CeraSGel

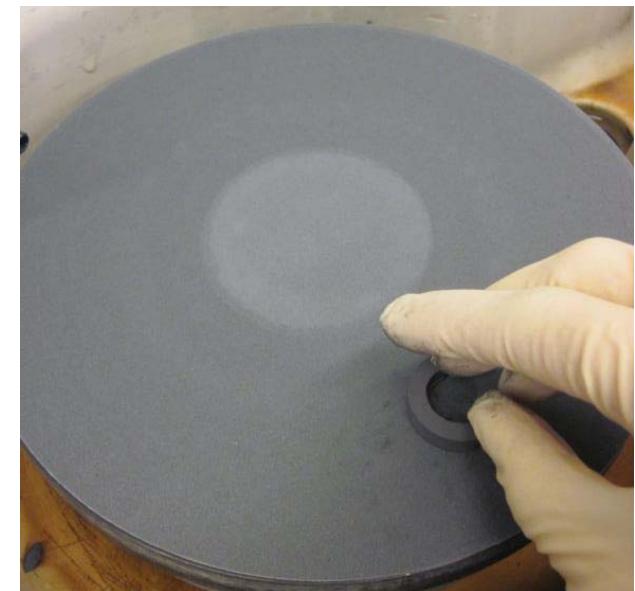
- 1 vol.% PVP
- 2 vol.% PVP
- 3 vol.% PVP

Polymer Content	pH	Estimated Yield Stress [Pa]
1 vol.%	$8.85 \pm 0.1$	567
2 vol.%	$8.91 \pm 0.1$	405
3 vol.%	$8.89 \pm 0.1$	235

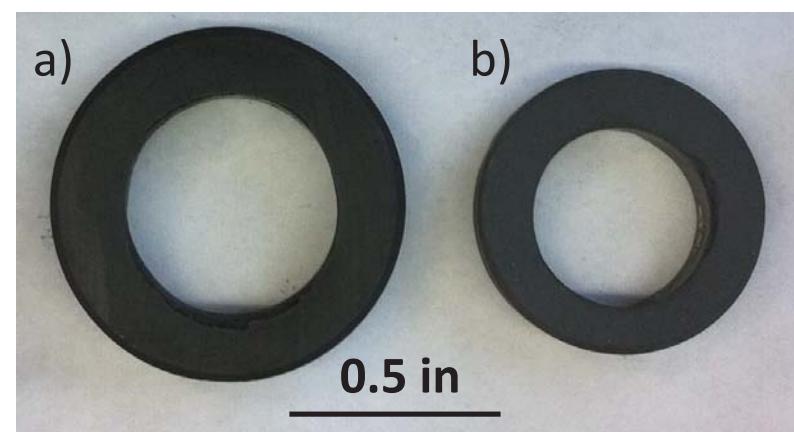
- pH of suspensions constant for PVP contents  
→ PVP content does not alter pH
- Time-dependent response
- Use creep test approach to approximate yield shear stress for  $\text{ZrB}_2 + \text{B}_4\text{C} + \text{WC}$  suspensions  
→ Yield stress decreases with increasing polymer content

# Machinable in Green State

- Prepare sample in green state
  - Even out surfaces by polishing
  - Chamfer edges
- **Binder burnout and pressureless sintering**
  - Ramp to 600°C (4°C/min), 1h hold (vacuum)
  - 1650°C (10°C/min), 1h hold, begin argon backfill
  - 1850 (10°C/min), 1.5h hold in argon



Preparing green body for mechanical testing.



a)  $\text{ZrB}_2$  sample in green state and b) after binder burnout and sintering.

# PVP Effect on Density and Internal Porosity

- Archimedes density test
  - True density (TD) = 6.17 g/cm<sup>3</sup>
  - Based on 86 wt.% ZrB<sub>2</sub>, 4 wt.% B<sub>4</sub>C and 10 wt.% WC

PVP content	Relative density (TD%)
1 vol.%	99.4 ± 0.3
2 vol.%	100.5 ± 0.4
3 vol.%	98.2 ± 0.8

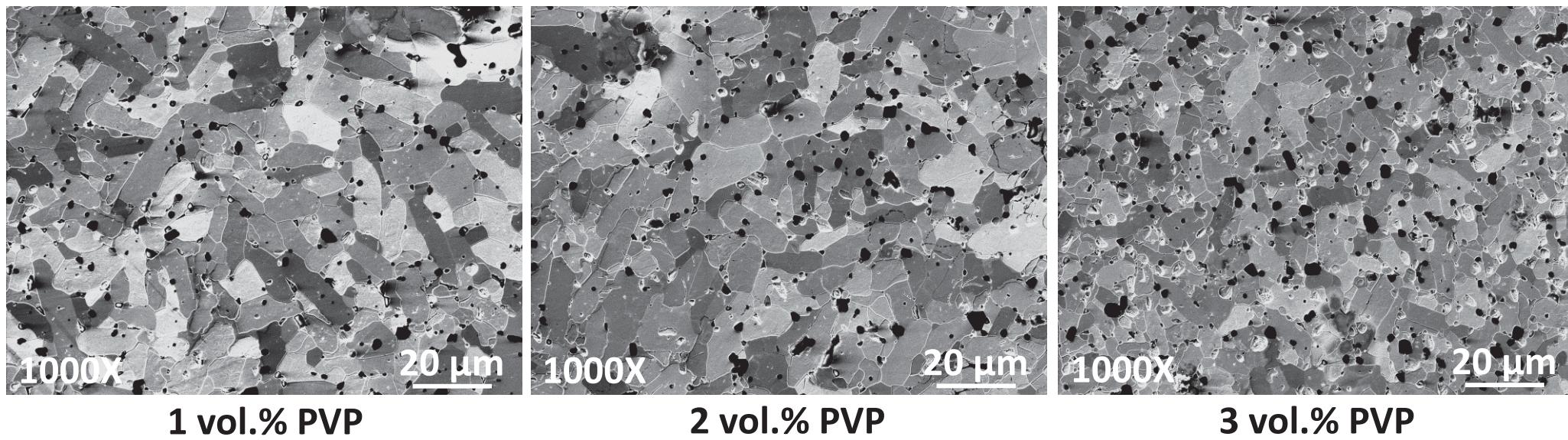
- Specimens prepared with 3 vol.% PVP had lowest density
- ~21% linear shrinkage

# PVP Effect on Density and Internal Porosity

## Scanning electron microscopy (SEM)

- Dense microstructure
- Grain size dependence

PVP content	Relative density (TD%)	Average grain size ( $\mu\text{m}$ )
1 vol.%	$99.4 \pm 0.3$	$9.8 \pm 6.2$
2 vol.%	$100.5 \pm 0.4$	$10.6 \pm 5.3$
3 vol.%	$98.2 \pm 0.8$	$7.7 \pm 3.7$

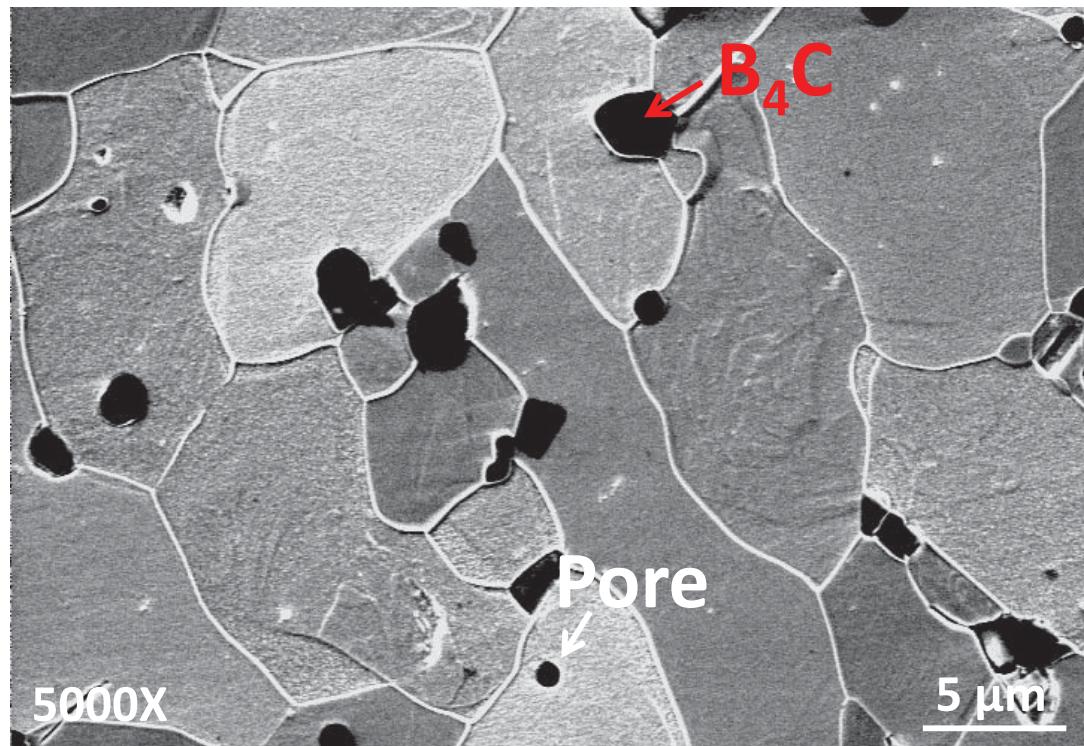


→Unclear if polymer content affects grain size of sintered part

# Elemental Analysis of Sintered Specimens

## Energy dispersive spectroscopy (EDS)

- $B_4C$  grains surrounded by  $ZrB_2$  grains
- No presence of oxygen detected



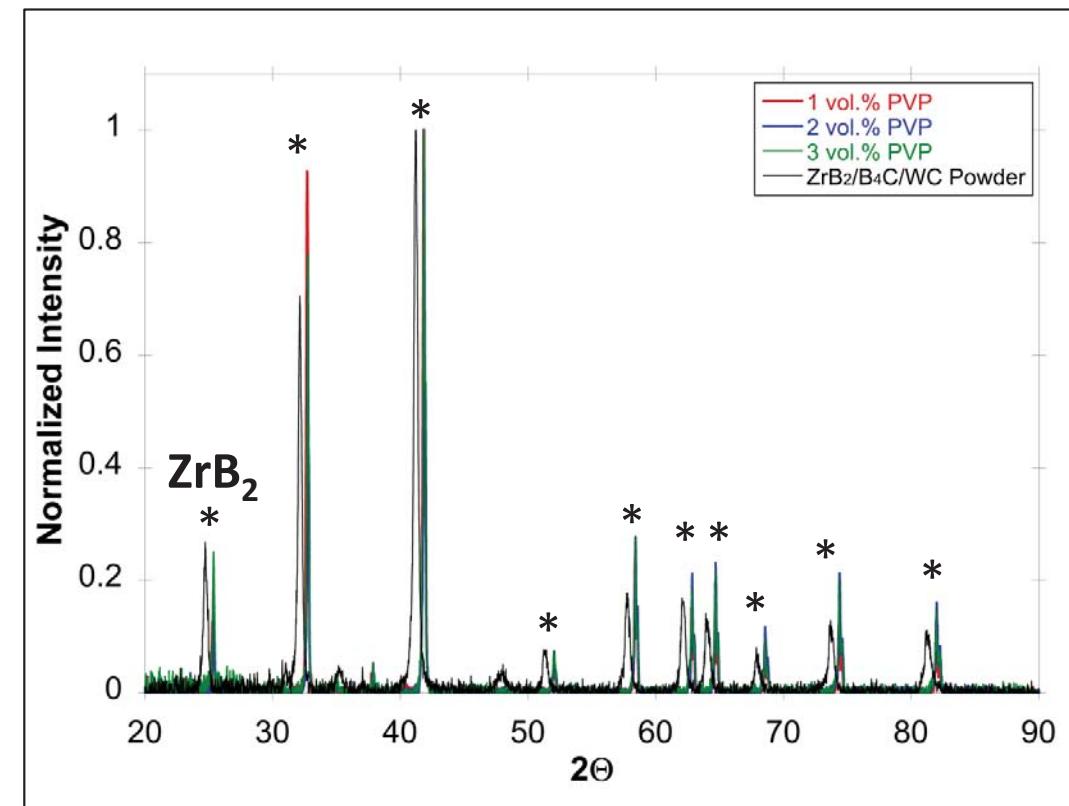
Cross section of specimen prepared with 1 vol.% PVP CeraSGel.

# Phase Analysis of Sintered Specimens

- Tungsten formed solid solution with  $\text{ZrB}_2$   
→  $\text{ZrB}_2$  peaks shifted to higher angles after sintering

- No oxide phases detected

✓ **Binder content did not seem to affect sintered ceramic compositions**



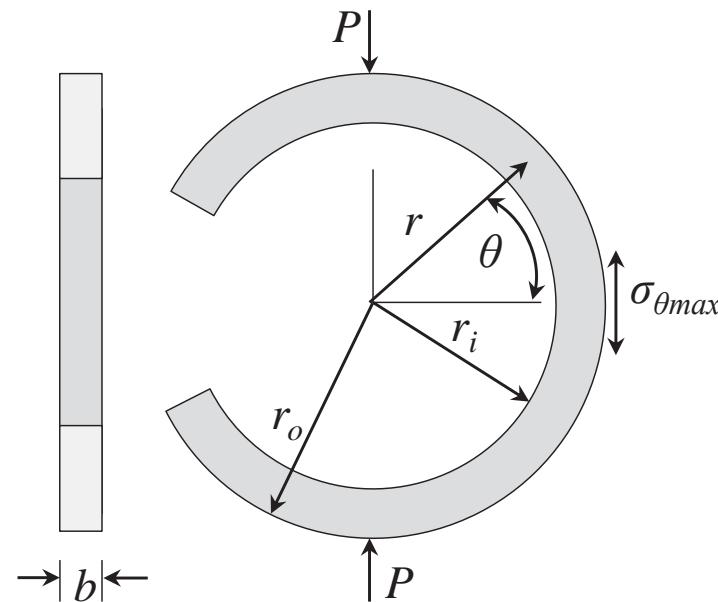
XRD spectra of sintered  $\text{ZrB}_2$  specimens prepared with 1, 2 and 3 vol.% PVP CeraSGels and of attrition milled  $\text{ZrB}_2/\text{B}_4\text{C}/\text{WC}$  powders.

# Mechanical Strength of Sintered Parts

ASTM C 1323-10<sup>1</sup>

Ultimate strength at ambient temperatures

- Requires compressive loading of C-ring specimens



$$\sigma_{\theta \max} = \frac{PR}{btr} \left[ \frac{r_o - r_a}{r_a - R} \right]$$

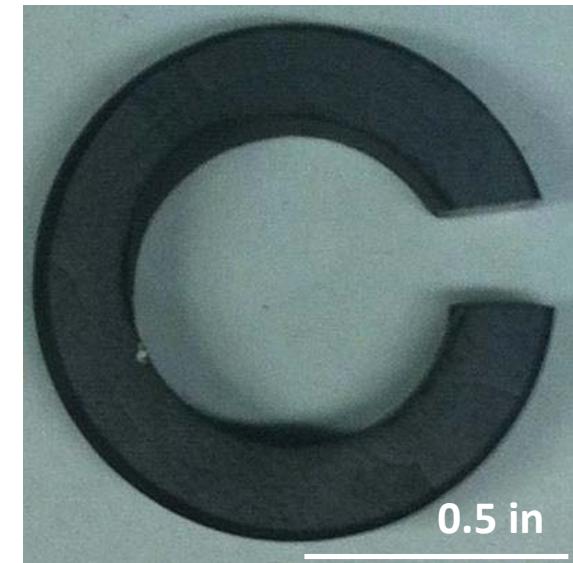
$$R = \frac{(r_o - r_i)}{\ln(r_o/r_i)} \quad r_a = \frac{r_o + r_i}{2}$$

Geometry of C-ring specimen for ASTM C 1323-10 (modified from standard<sup>1</sup>).

# Effect of PVP on Average C-ring Strength of ZrB<sub>2</sub> Samples

- C-ring strength values lower than anticipated
  - ASTM C 1323-10 not comparable to other flexure tests
- Grain sizes comparable to literature
- Defects introduced during forming

PVP Content in vol.% (wt.%)	Relative density (TD%)	Average C-ring strength (MPa)
1 (0.3)	99.4 ± 0.3	<b>31 ± 12</b>
2 (0.7)	100.5 ± 0.4	<b>73 ± 15</b>
3 (1.0)	98.2 ± 0.8	<b>75 ± 27</b>



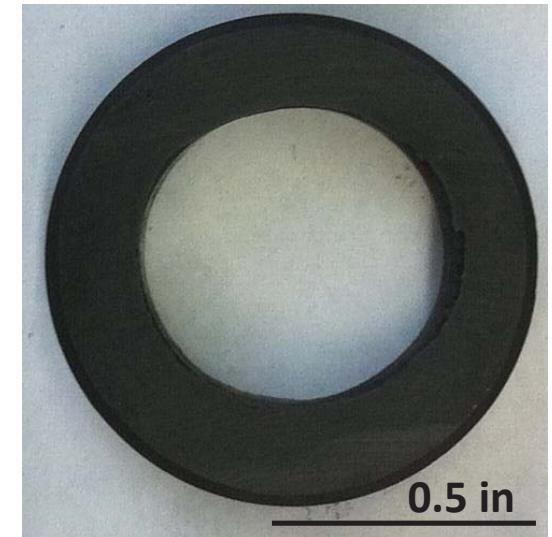
Final sintered C-shaped sample.

→ Evaluate ZrB<sub>2</sub>-based CeraSGels with varying PVP contents and powder loadings

# Conclusions and Future Work

- **Rheology of ZrB<sub>2</sub>+B<sub>4</sub>C+WC CeraSGels**
  - Flow properties suitable for room-temperature processing
  - Effective yield point decreased with increasing PVP content
- **Machinable in green state**
- **Dense (>98%TD) ZrB<sub>2</sub> samples produced by pressureless sintering**
  - 21% linear shrinkage
  - PVP did not affect final composition
- **Mechanical characterization using ASTM C 1323-10**
  - C-strength increased with increasing PVP content

→ Prepare and evaluate CeraSGels and resulting C-ring specimens containing >3 vol.% PVP with varying solids loading



Dense ZrB<sub>2</sub> rings have been fabricated by room-temperature injection molding of CeraSGels.